

Breakthrough of a Long Tunnel by Geological Evaluations Combined with Various Types of Forward Exploration

— Hokuriku Shinkansen New Hokuriku Tunnel (Okunono Construction Area)—

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1. Introduction

The Hokuriku Shinkansen is a 690 km-long line that starts in Tokyo and ends in Osaka City via Nagano, Toyama, and Obama. The Okunono section of the New Hokuriku Tunnel is a 4,880-meter-long middle section of a 20 km-long mountain tunnel located in Fukui prefecture. Construction was done using a working pit (inclined shaft). The cross-section of the excavation was approximately 70 m², using the full-sectional method with an auxiliary bench. Digging was done by blasting method, with continuous belt conveyor method used for shedding. Eleven faults were expected in the construction area (shown in Fig. 1), with widths ranging from a couple of meters to maximum 80 m. The natural ground was expected to be fragile with many fractures developed along the faults, with concerns of sudden water inflow especially in the area of chert.

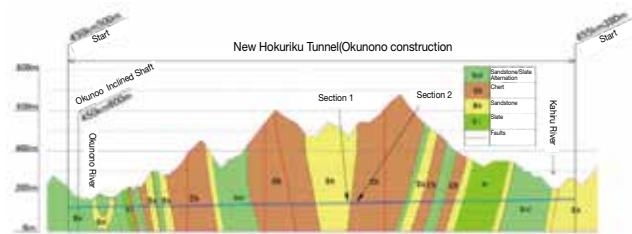


Fig. 1 Longitudinal Profile of the Geology

2. Overview of Exploration Methods

As shown in Table 1, three types of forward exploration were carried out to understand the geological conditions in front of the cutting face.

Tab. 1 List of Forward Probe

List of Forward Probes			Notes
Name	Probe depth/number	Results	
medium-length non-core exploration drilling	150-180m/time 34 times (full length)	Index-value of energy	Down-the-hole method Water-pressure hammer boring
short-length non-core exploration drilling	30-50m/time 120 times (full length)	Speed ration of normalized drilling Prediction of water inflow	Percussion drilling
Seismic Survey	150-180m/time 33 times (full length)	Prediction of water inflow	TSP203
		Reflection surface V_p/V_s ratio	

3. Prediction of Natural Ground using Forward Exploration Results and Actual Digging Results

Conditions of the natural ground 150 m ahead were predicted by combining result from the non-core exploration drillings and in-pit elastic wave survey described above. The results showed multiple sections of fragile terrain including fault fracture zones, fracture concentration zones, and stratigraphic boundaries, as well as sections with high risk of sudden and heavy water inflow. Among the potentially bad sections, the following two (Fig. 1) were unique in the way they clearly showed the characteristics from the forward exploration results.

Section 1: 453km185-215m (L=30m)

Section 2: 453km250-265m (L=15m)

Table 2 is a comparison between predicted and actual natural ground conditions for sections 1 and 2.

Tab. 2 Expected and Actual Conditions of Natural Ground

	Kilometrage	Short to Medium-scale non-core drilling logging	Seismic Survey	Condition of Natural Ground	
				Expected	Actual
Section 1	453km 185 ~ 215 m	Chert dominated ground Equivalent to IS - IN-1 Water: 1,000L/min Water pressure: 0.75MPa	VP downward Focus on reflection surface V_p/V_s reduce	Mainly chert Cracks, exfoliation, and other surface discontinuities is significant Possibility of water high due to being a valley	Mainly fragile chert Face of digging had a lot of sediment and caused much exfoliation Digging face had 40L/min water at maximum
Section 2	453km 250 ~ 265 m	Chert and Alternation mix Equivalent to IS to IN-2 Water: 450L/min	Lot of change in V_p Dense reflection surface V_p/V_s slightly changed	Mix of chert and sandstone/slate alternation A lot of cracks, exfoliation, and other discontinuities Low possibility of high-level water inflow	Mainly chert with many cracks Excavation face could not stand alone Digging face had water 20L/min at maximum

3-1 Section 1: 453km185 ~ 215m

This section raised concern of sudden water inflow. The water inflow rapidly increased to 1,000 L/min. during logging. Additional measurements of the inflow rate and inflow pressure were done. Judging from the results, due to the predominantly fractured chert soil, there was a very high possibility that a large amount of water inflow would occur when the tunnel face was reached.

The actual site was dominated by fragile chert, and the maximum water inflow was 40 L/min. at the mirror surface. A lot of the dirt showed sedimentation especially on the face of the excavation with many fission exfoliation shown in Photo 1.

The water inflow from drilling and logging holes decreased from 1,000 L/min. to 500 L/min. as the face progressed, and the water inflow on the mirror surface during excavation was minimized by draining water in the forward ground using medium-scale drilling and logging.

3-2 Section 2: 453km250 ~ 265m (L=15m)

This section was feared to be fractured ground. Combining results of various tests, unstable ground was expected to be located near the boundary between the multi-fractured chert and the soft sandstone/slate alternation.

The actual ground was a multi-fractured chert ground with small water inflow, but as seen in Photo 2, the small amount of water caused the face to be very unsustainable.

In the actual construction, the core was left during excavation to stabilize the mirror surface. The water inflow at the face was minimized by draining water during drilling.

4. Conclusion

Bad ground conditions were predicted in advance with a high degree of accuracy by evaluating the ground using a combination of various types of frontal surveys. The excavation was conducted safely without any delays by considering appropriate support patterns and auxiliary construction methods beforehand as well.

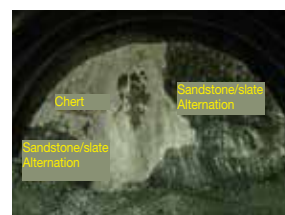


Photo 1 Face Condition (453km200m)

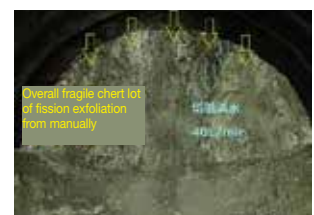


Photo 2 Face Condition (453km260m)